



## Road Load Data Acquisition Committee

SAE FD&E  
4-5 April, 2000

### Minutes

#### Current Activities:

- Rainflow Standard - closed
- Time History format - closed
- ASCII data for web page - Andrew Whelan
- Statistical Data Analysis
- ATV contributions

#### Today's Presentation Session:

- Non-Stationary Random Load Modeling
- Discussion on RLDA contributions to ATV project



## Modeling of non-stationary variance in vehicle loading histories for fatigue analysis

SAE FD&E Spring 2000  
4-5 April, 2000

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Professor Surot Thangjitham, Virginia Tech

Professor Norman Dowling, Virginia Tech





### Concise fatigue load description



$$\mathbf{x}_t = \mathbf{s}_t \mathbf{n}_t$$



#### Motivation:

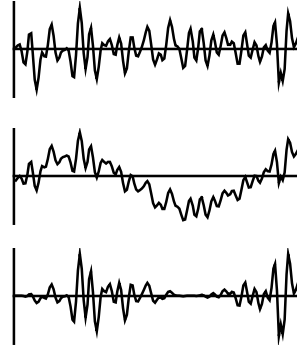
- storage reduction
- test machine / FEA compatibility
- monitoring
- concentration on relevant content
- elimination of non damaging events
- manipulation
  - superposition
  - extrapolation





## General Random Fatigue Loads

- Stationary
- Nonstationary  
in mean  
and / or  
in variance



## Model for Nonstationary Fatigue Loading:

$$x(t) = s(t) n(t)$$

$s(t)$  ... variance scaling function

$$s_t^{BC} = \frac{1}{2} c_0 + \sum_{k=1}^{M_s} [c_k \cos(\omega_0 k t \Delta t) + d_k \sin(\omega_0 k t \Delta t)]$$

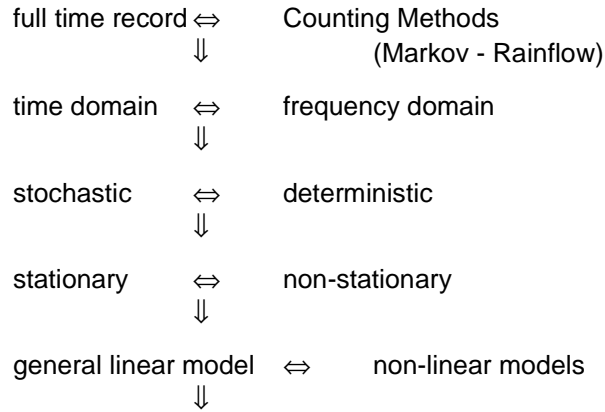
$n(t)$  ... zero mean, stationary noise content

$$n_t - \phi_1 n_{t-1} - \dots - \phi_p n_{t-p} = e_t - \theta_1 e_{t-1} - \dots - \theta_q e_{t-q}$$





### Data Reduction Schemes



### ARMA model

$$n_t - \phi_1 n_{t-1} - \dots - \phi_p n_{t-p} = e_t - \theta_1 e_{t-1} - \dots - \theta_q e_{t-q}$$



<i>Modeled</i>	<b>Characteristics of ARMA Method</b>	<i>Not Modeled</i>
Dynamics		Rainflow Cycles
Auto-Cross-Correlations		Extremes
<b>Advantages</b>	<b>Fundamental</b>	<b>Disadvantages</b>
Stochastic Description (Ensemble)		"Involved" Model Building
Consistent Multichannel Extension		Not Same Rainflow Cycles
Continuous Nonstationarity Description		Not Identical Extremes
Concise Description		
Simple, Fast Simulation		





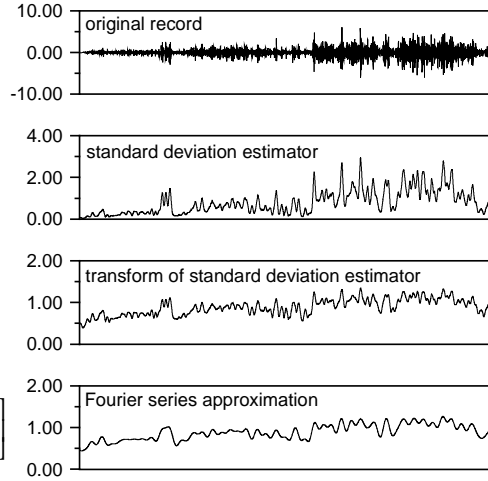
### Reconstruction Procedure

$$x_t = s_t \cdot n_t$$

$$\tilde{\sigma}_t^2 = \sum_{j=0}^n w_{j-\frac{n}{2}} x_{t+j-\frac{n}{2}}^2$$

$$\tilde{\sigma}_t^{BC} = \begin{cases} \tilde{\sigma}_t^\lambda & \text{for } \lambda \neq 0 \\ \log \tilde{\sigma}_t & \text{for } \lambda = 0 \end{cases}$$

$$s_t^{BC} = \frac{1}{2} c_0 + \sum_{k=1}^M \left[ c_k \cos(\omega_0 k t \Delta t) + d_k \sin(\omega_0 k t \Delta t) \right]$$

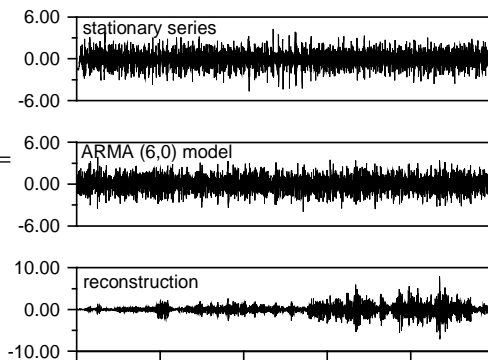


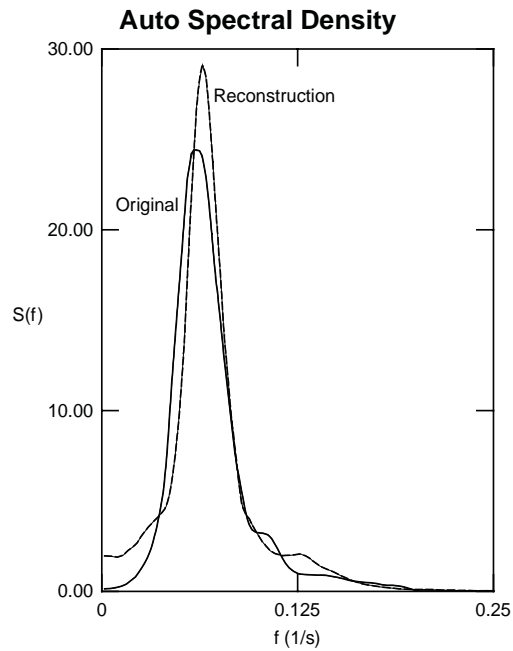
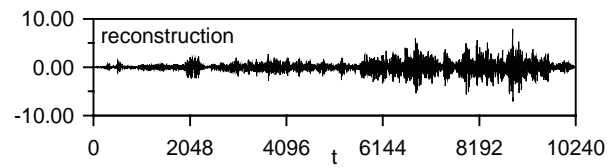
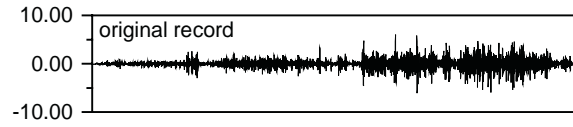
### Reconstruction Procedure

$$x_t / \sigma_t = n_t$$

$$n_t - \phi_1 n_{t-1} - \phi_2 n_{t-2} - \dots - \phi_p n_{t-p} = a_t - \theta_1 a_{t-1} - \theta_2 a_{t-2} - \dots - \theta_q a_{t-q}$$

$$x_t = s_t \cdot n_t$$





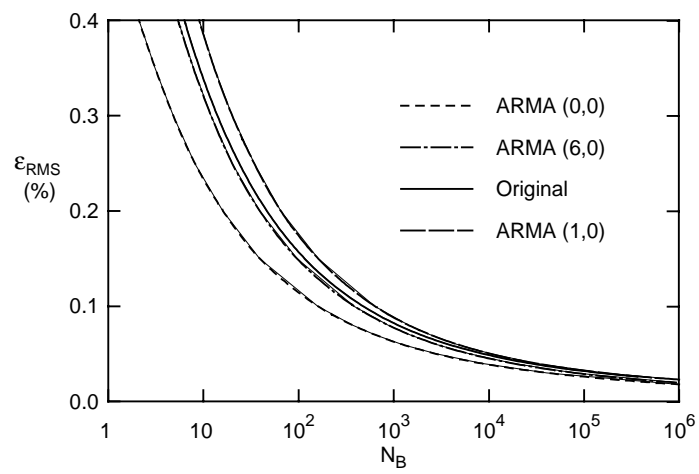


## Fatigue Life Calculation

- RMS scaling factors
- Rainflow Count
- Local Strain Approach
- Palmgren Miner Rule



## Fatigue Life





### Ensemble Generation

$$s_r^{N_z} = \frac{1}{2}c_0 + \sum_{k=1}^M \left[ c_k \cos(\omega_0 k t \Delta t - \gamma_k) + d_k \sin(\omega_0 k t \Delta t - \delta_k) \right]$$

$$\gamma_k, \delta_k = \begin{cases} U & \text{for } k \in (N_z + 1, M) \\ 0 & \text{for } k \in (0, N_z) \end{cases}$$

