



WCX APRIL 9-11
2019
DETROIT

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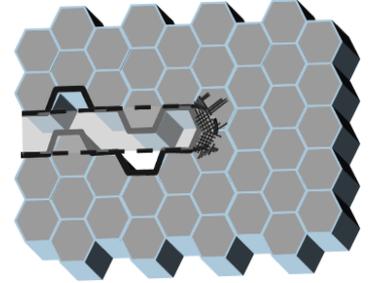
SAE FD&E Total Life Project Overview

Dan Lingenfelter, nCode Federal LLC

SAE FDE

Total Life Project and Total Life (WholeLife) Method

- **Contributors**
- **Background – Why total life is significant**
- **Status and future work**
- **Total life method - Fundamental concept**
- **Summary**



Engineering is the art of modeling materials we do not wholly understand, into shapes we cannot precisely analyze, so as to withstand forces we cannot properly assess, in such a way that the public has no reason to suspect the extent of our ignorance.

Dr. A.R. Dykes, Chairman, British Institute of Structural Engineers

Industry

- B & W Trailer Hitches
- Caterpillar
- Deere and Company
- MTS
- Hendrickson Trailer Suspensions
- Element Materials Technology
- Trilion Quality Systems
- Lambda Technologies
- Hill Engineering
- nCode (Prenscia)

Academia

- Mississippi State University
- Kansas State University
- University of Windsor
- University of Waterloo
- Carleton University

- **Historically FDE has championed strain life methods**
- **More recently FDE recognized need to better evaluate useful life**
 - Total Life project initiated by Tom Cordes in 2012
- **Total Life Projective Objectives:**
 - Develop set of test results to evaluate life prediction methods
 - Evaluate unified theory of fatigue developed by prof. G. Glinka
 - Evolving technology that is now ready for production application
 - Develop improved measure of useful life than cycles to initiation
 - Provide ability to quantify improvements in the life of weldments due to geometry and residual stress

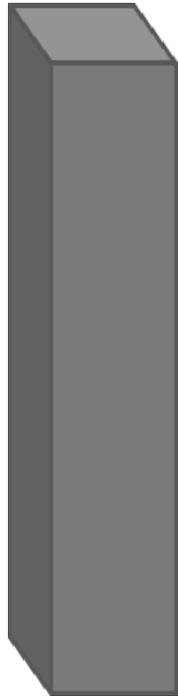


Project Tasks

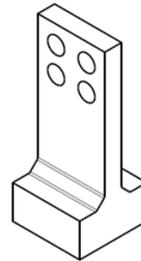
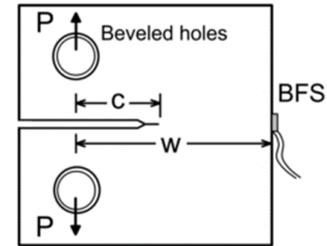
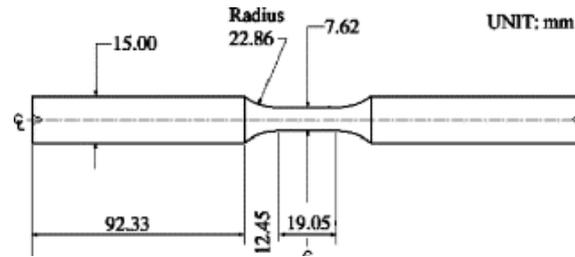
- **Planning, Organization & Leadership**
 - Specimen Design, Procurement, Documentation
- **Strain-life, Crack Growth Testing, And Strain Measurements**
- **T-joint Component Finite Element Analysis**
- **Machined & Welded T-joint Component Fabrication**
- **T-joint Component Fatigue Testing**
- **Residual Stress Distribution Simulation And Measurement**
- **Striation (Marker Band) Measurements And Fractography**
- **Fatigue Life Predictions And Correlation To Test Data**
- **Documentation**
 - Science not documented is science not done



Procured 80 feet of 4" x 4" RCS A36 HR bar



Microstructure, Chemistry & Hardness Sample



- Challenging material for crack growth
- Both fully machined and welded test samples

Participants

Tom Cordes (Project Champion)

Stephen Horstemeyer

Jonathan Pickworth

Semyon Mikheevskiy

Stephanie Swanson

Grzegorz Glinka

James Patterson

Sergey Bogdanov

Narendra Singh

Phil Dindinger

N. Jayaraman

William Ulrich

Adrian DeWald

Brandon Evans

Chad Kerestes

Charlie Sieck

Doug Hornbach

Matt Campbell

Peter Huffman

Brian Dabell

Eric Johnson

Hayley Brown

Jeff Mentley

Mary Wickham

Rakesh Goyal

Taylor Jones

Vipul Shinde

Casey Gales

Eric Norton

John Goldak

Justin Mach

David Griffith

Lingyun Pan

Mike Lister

Paul Prevey

Perry Mason

Ryan Blodig

Timothy Vik

Randy Peck

Steve Haeg

Al Conle

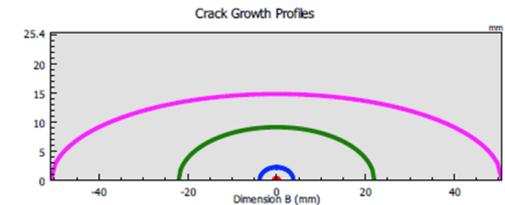
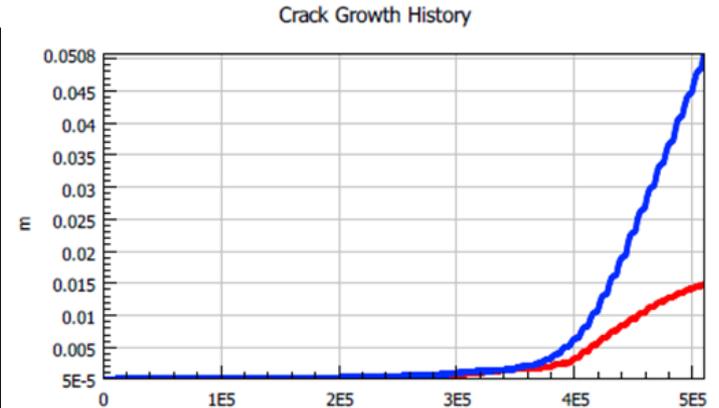
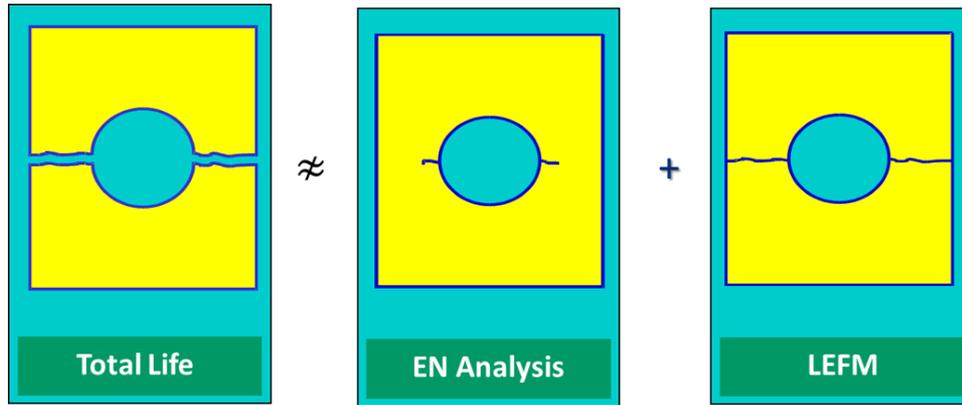
- **Developed high quality material properties**
- **Fabricated and tested “components”**
 - Six different loading histories
 - Thirty tests completed to date
 - 13 machined & 17 welded samples
 - Additional test articles ready to test
- **Residual stress measured and compared to simulations**
 - Work continues to resolve differences
- **Life predictions complete**
- **Following papers provide details and documents results to date**

Following papers document Total Life Project

- **FD&E Total Life T-sample Residual Stress Analytical Predictions And Measured Results**
- **Fatigue Life Prediction For F.D.E. Welded Plate Specimen**
- **Testing Of Welded And Machined A36 Steel T-joint Configuration Specimens**
- **Comparison Of Total Fatigue Life Predictions Of Welded And Machined A36 Steel T-joints**
- **Accounting For Geometry And Residual Stresses In Weld Fatigue: A Strain Energy Density Approach To Total Life Of Welded T-specimens**
- **A Finite Element Based Methodology For Combined Crack Initiation And Crack Growth Prediction In Welded Structures**
- **For latest results and information on the FD&E; visit www.fatigue.org**

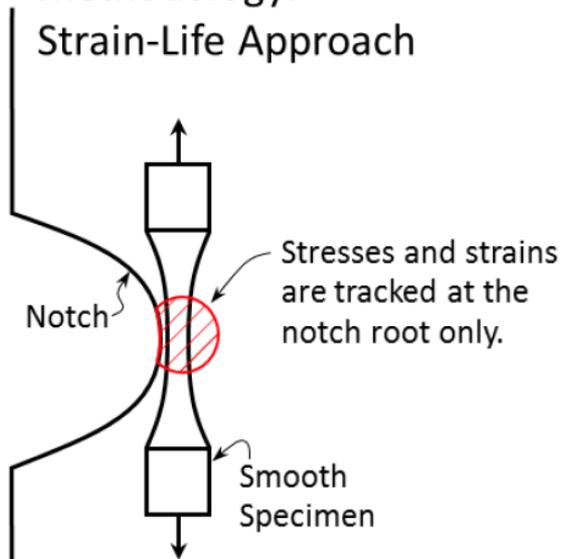
Total Life Method \approx Crack Initiation + Crack Growth

“The idea of splitting the fatigue life into the initiation and propagation stages is very useful in practice, although the distinction between the stages is still under discussion.” G.Glinka - 1986



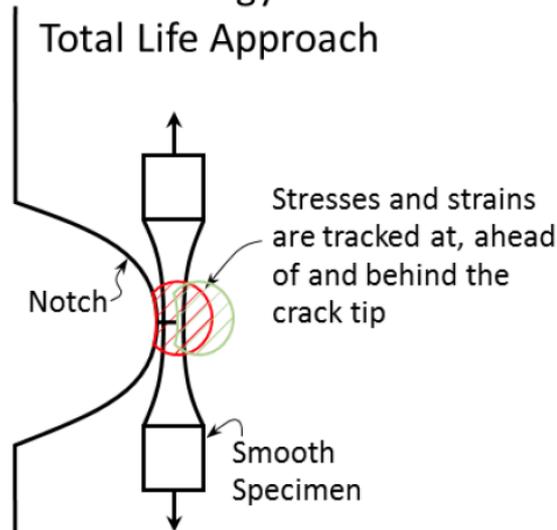
Total Life Method is much different than simply $N_i + N_p$

Methodology: Strain-Life Approach



Stress-strain cycles are then taken into a cycle by cycle local strain linear Miner's damage rule analysis to calculate the fatigue life to "crack initiation".

Methodology: Total Life Approach

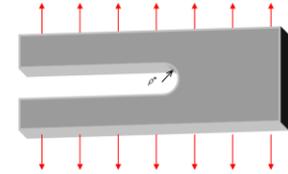
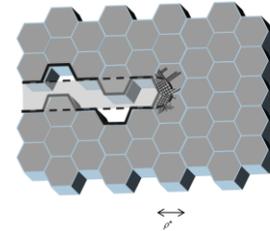


Stress distribution cycles are then taken into a cycle by cycle fracture mechanics da/dN vs Total Driving Force analysis to calculate the fatigue life to "crack initiation" + "crack propagation".

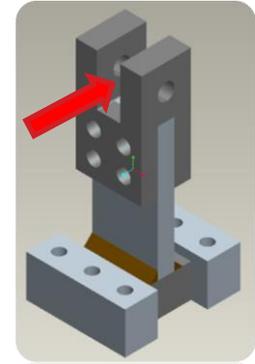
AKA - Unified Theory of fatigue (UniGrow)

Developed by Prof. G. Glinka,

University of Waterloo, Canada



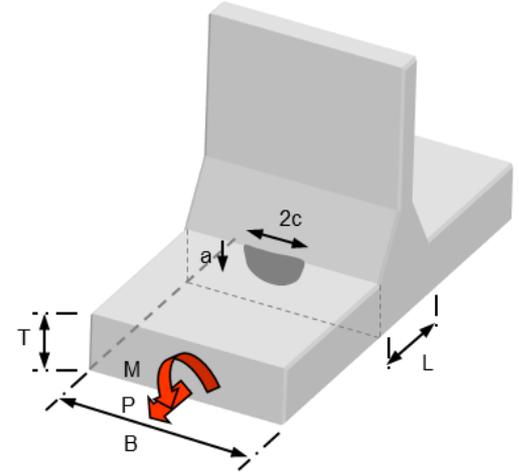
- **Radius at tip not a singularity – radius = ρ^* (Rho star)**
- **Radius enables use of Neuber to determine local stress and strain plasticity**
- **Track cyclic local stress-strain ahead and behind crack “tip”**
- **Universal weight functions used to determine stress intensity into the plate and along surface**
- **Enables superposition of applied and residual stresses**
- **Repeated initiation at crack tip radius**
- **Delta kappa is driving force**



$$K = \sigma C_f Y \sqrt{\pi a} + K_r$$

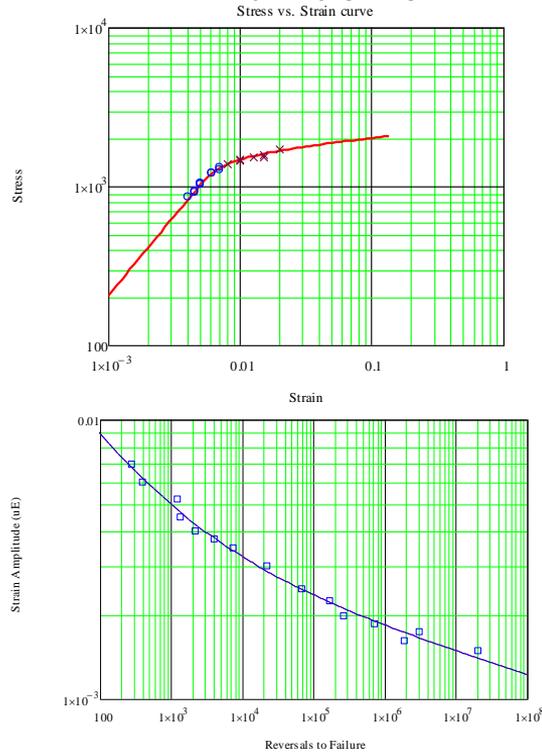
$Y = f(\text{geometry, stress profile})$

- Transforms nominal stress into Stress Intensity (SI) at the crack tip
- UWF applies stress profile explicitly of the geometry (i.e. use a single geometry for any number of stress distributions)
- UWF can deal with complex stress distributions such as residual stress fields and crack-tip wake stresses

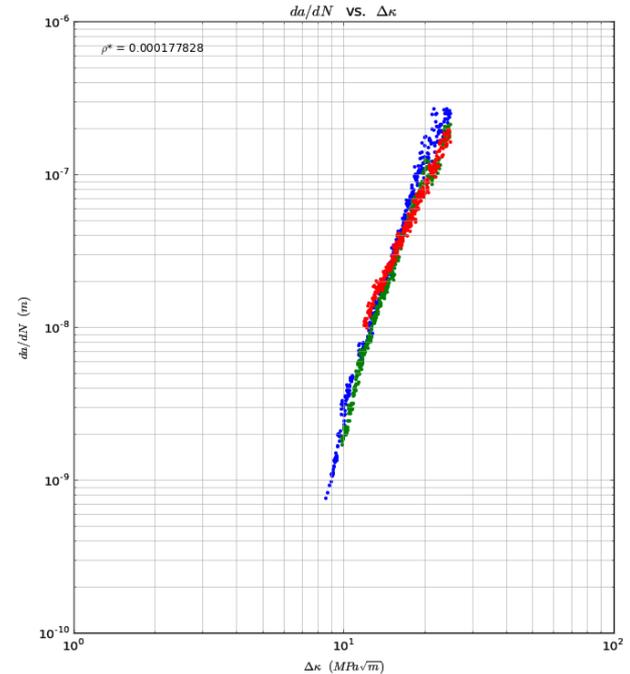


Total Life Inputs

Strain-Life (EN) properties

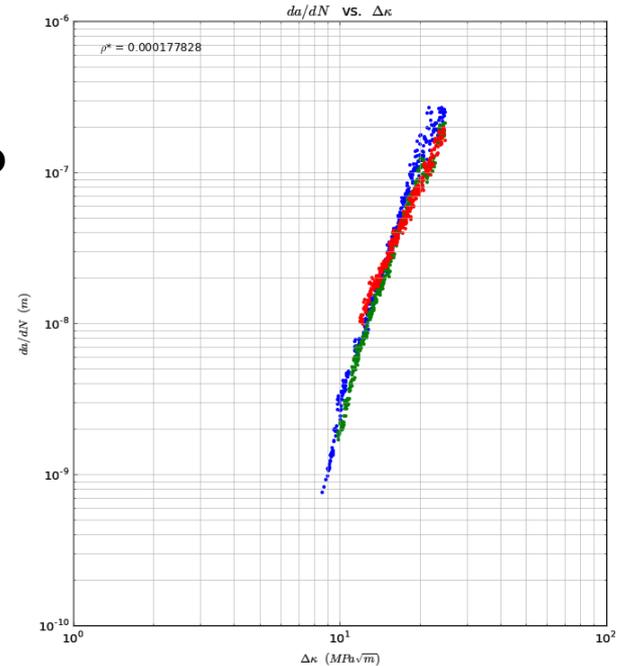


LEFM crack growth properties da/dN vs delta Kappa



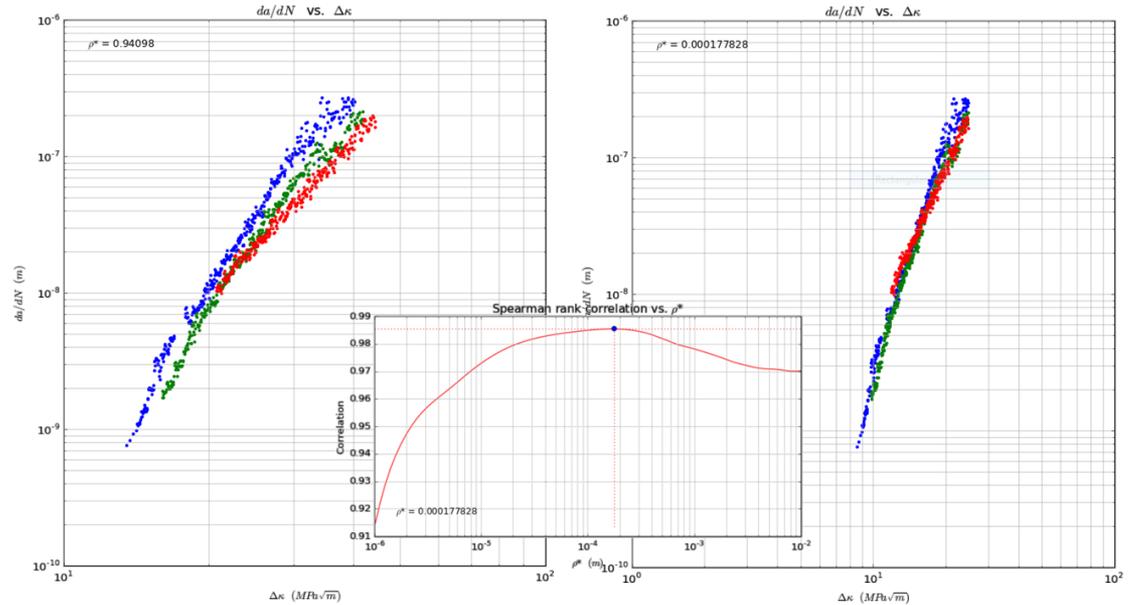
Crack Growth Model da/dN vs $\Delta\kappa$

- Crack growth rate da/dN is a function of the 'crack-tip driving force'; $\Delta\kappa \frac{da}{dN} = C\Delta\kappa^m$
- $\Delta\kappa$ is a function of the 'stress intensity' and R ratio (after Walker); $\Delta\kappa = K_{max}^p (K_{max} - K_{min})^{1-p}$
- K is a function of stress σ , geometry Y , crack length a , and the residual stress field at the tip of the crack K_r ; $K = \sigma C_f Y \sqrt{\pi a} + K_r$
- C_f is the 'small crack correction'; $C_f = \left(1 + \frac{1}{2} \sqrt{\frac{\rho^*}{a}}\right)$



Estimating $\frac{da}{dn}$ vs ΔK and ρ^*

Collapse crack growth curves at multiple R ratios to collapsed segmented curve while optimizing regression coefficients



Un-collapsed curve

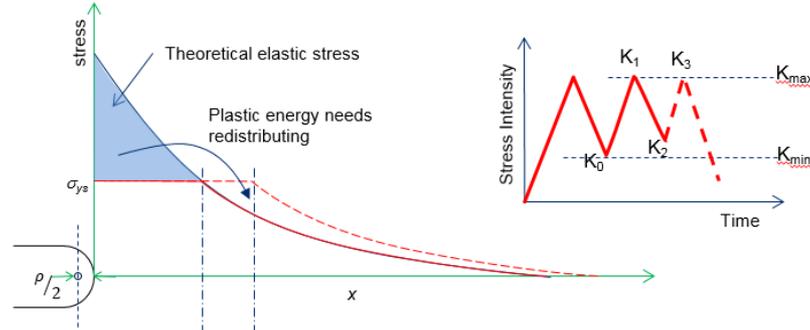


Collapsed curve

Cyclic Crack-tip Plasticity Model K_r ... Estimating local stress

Crack-tip opening

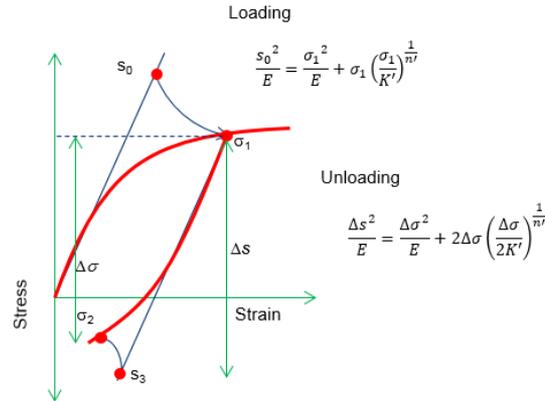
$$\overrightarrow{K_0 K_1}$$



Crack-tip closing

$$\overrightarrow{K_1 K_2}$$

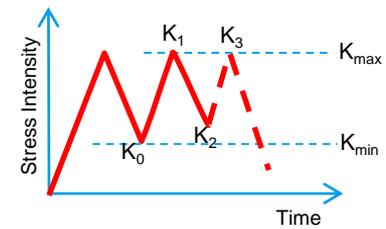
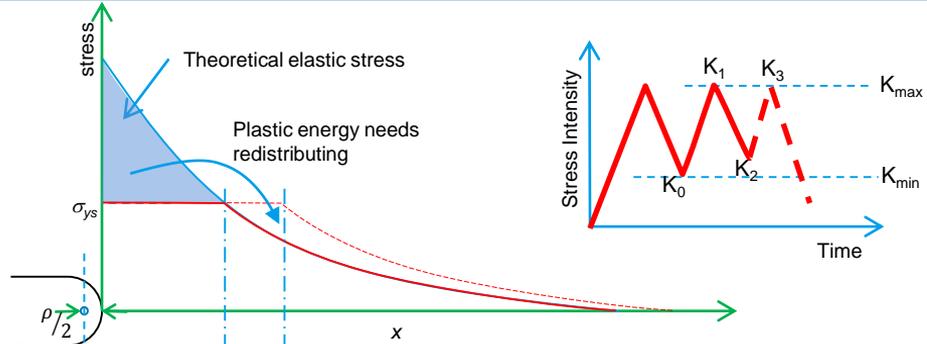
Crack-tip plasticity is based on multiaxial Neuber-Ramberg-Osgood cyclic plasticity model with plastic redistribution:



Cyclic Crack-tip Plasticity Model K_r

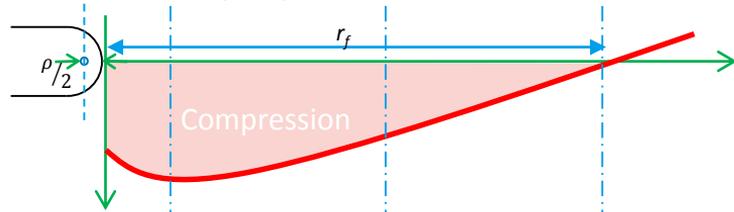
Crack-tip opening

$$\overrightarrow{K_0 K_1}$$

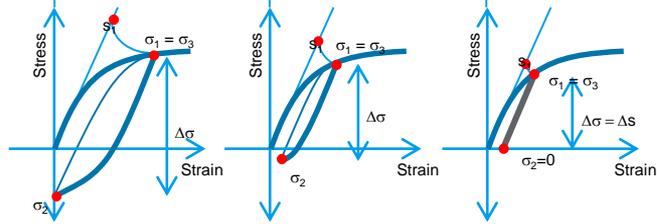


Crack-tip closing

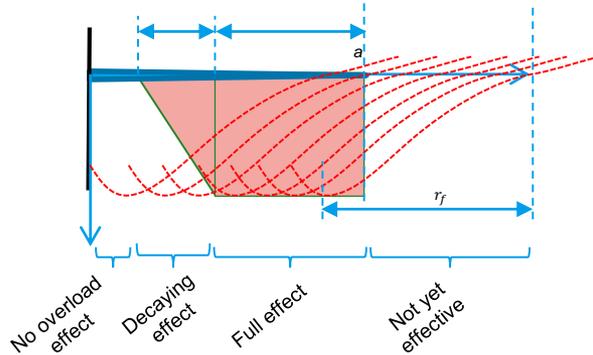
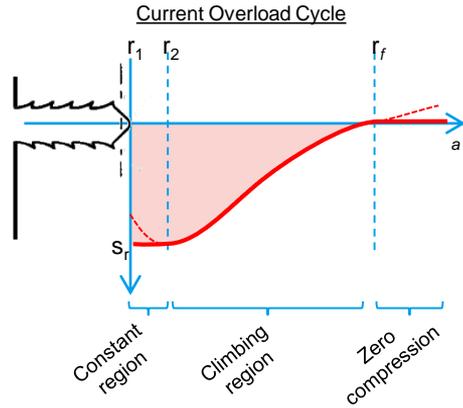
$$\overrightarrow{K_1 K_2}$$



Crack-tip plasticity is based on multiaxial Neuber-Ramberg-Osgood cyclic plasticity model with plastic redistribution:



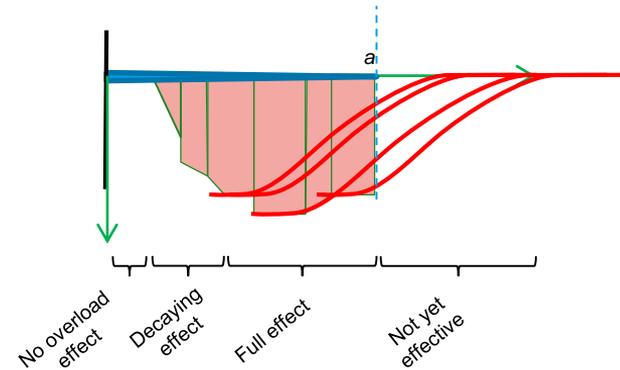
Cyclic Crack-tip Plasticity Model K_r - Crack retardation



Compressive wake from constant-amplitude loading



Compressive wake from variable-amplitude loading



Summary

- **Strain life serves us well but it doesn't quantify useful life**
- **Total life provides a better measure of useful life**
- **Crack size vs cycles better defines useful life than cycles to initiation**
- **Total life provides ability to quantify improvements in the life of weldments due to geometry and residual stress**

Supporting details for this summary are
in the referenced papers presented in
this session

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- **Crack Initiation and Propagation Fatigue Life Prediction for an A36 Steel Welded Plate Specimen**

Thank you

- Dan Lingenfelser
- nCode Federal LLC
- 100 Research Blvd, Suite 216, Starkville, MS
- 248-854-7946
- Dan.Lingenfelser@ncodefederal.com